



VFD Overcurrent Fault and Motor Overload – Causes & Fixes

Variable Frequency Drives (VFDs) are critical in controlling motor speed and torque in industrial systems. However, they must also protect themselves and motors from electrical and mechanical stresses. Two common protective trip conditions in low-voltage AC drives (and similarly in DC drive systems) are **overcurrent faults** and **motor overloads**. This article explains what these terms mean in the VFD context, why they occur, and how to address their root causes. We focus on practical scenarios (conveyors, pumps, fans, etc.) in low-voltage and DC drive applications, with references to industry standards (IEC 61800, NEMA MG-1) and guidance from major manufacturers (ABB, Hitachi, Eaton, Yaskawa, Lenze). Real-world case studies are included to illustrate problems and solutions, complete with baseline vs. resolved metrics.

Understanding Overcurrent Faults vs. Motor Overload in VFDs

Overcurrent Fault (OC Fault): In VFD terminology, an *overcurrent fault* is typically an **instantaneous** or very rapid surge of current beyond the drive's safe limit. The VFD will immediately shut down ("trip") to protect itself and the motor when this occurs ¹. Unlike an external circuit breaker that might trip on any overcurrent, the VFD's internal OC fault threshold is usually set high (often ~250–350% of the drive's rated current) ². For example, ABB's ACS880 drives trigger an F001 overcurrent fault when output current exceeds about 2.5–3.5× the drive rating ². This level is not adjustable by the user – it's a hardware protection to prevent IGBT or power circuit failure ³. In essence, an OC fault means **"something caused a huge spike in current, and the drive intervened immediately."**

Motor Overload: *Overload* refers to a *sustained* over-current condition that overheats the motor (and possibly the drive) over time. Rather than a sudden spike, an overload develops when current stays above the motor's rated level for too long. VFDs include electronic thermal modeling (often an **I²t** algorithm) to estimate motor heating ⁴ ⁵. If the motor draws high current beyond its allowable service factor or time limit, the VFD will trip on a motor overload fault to protect the motor windings from insulation damage ⁴ ⁶. For example, Hitachi's WJ200 VFD shows error "E05 – Overload protection" when its electronic thermal sensor detects a motor overload and shuts off output ⁶. In many VFDs, "motor overload" corresponds to what an old-fashioned thermal relay or fuse would do – it's essentially an **overheat protection** for the motor (sometimes labeled OL1 or OL2 in drive fault codes).

Overcurrent vs Overload: These terms are related but not identical. Any overload condition causes overcurrent, but not all overcurrent events are due to overload ⁷. Think of *overload* as a subset of overcurrent: an overload is when excessive load on the motor causes current above its rating (e.g. a 50 A motor drawing 60 A continuously – that's an overload). In contrast, an *overcurrent fault* in a drive often implies a more abrupt fault condition (like a short-circuit or locked rotor surge) that exceeds the instantaneous threshold. In practice, **VFDs differentiate the two:** an OC fault (instant spike) versus an overload trip (time-dependent heating). Many drives have separate fault codes for each. For instance, Yaskawa drives use "OL1" for motor overload and reserve "OC" or similar code for instantaneous overcurrent ⁸ ⁹.



Understanding this distinction is important: An overcurrent fault typically points to a **sudden event** or severe issue (electrical fault or abrupt mechanical jam), whereas a motor overload suggests a **sustained condition** of excessive load or inadequate cooling. Next, we will explore the causes of each and how to fix them.

Causes of VFD Overcurrent Faults

Overcurrent faults can occur in various scenarios where the motor or drive experiences a sudden demand for current beyond its capacity. Below are common causes of OC faults, along with explanations:

- **Mechanical Binding or Jamming:** One of the most frequent causes of instant overcurrent is a **stalled or jammed motor**. If the driven machinery is stuck (e.g. a conveyor jam, a pump with a clogged impeller, a seized bearing), the motor can rapidly draw a very high current (approaching locked-rotor amps) while trying to overcome the blockage ¹⁰ ¹¹. This sudden current surge often exceeds the drive's limit, tripping a fault in milliseconds. In real terms, a motor under stall can pull 5–8 times its rated current, which will almost certainly trigger the VFD's 250–350% threshold ². **Fix:** Immediately **inspect the mechanical system** for jams, obstructions, or binding. Clear any jams and verify the motor and load rotate freely by hand ¹² ¹³. Check for adequate lubrication and replace faulty bearings or couplings if needed. In a case at a **packaging plant**, a conveyor kept tripping on OC fault – baseline current spiked to ~300% when jammed. After installing a sensor to detect package backup and halting the feed when a jam is imminent, the peak current was reduced to ~120% of rated and OC trips were eliminated. Preventive maintenance (keeping the conveyor clean, properly tensioned, and aligned) further avoided recurrent jams.
- **Short Circuit in Motor or Cables:** An electrical short on the VFD output – either phase-to-phase or phase-to-ground – presents a very low impedance path, causing an abrupt overcurrent. This might be due to damaged motor winding insulation or a pinched output cable. If a phase-to-ground short occurs, many drives will report a ground fault, but a severe phase-phase short will trip an overcurrent fault almost immediately ¹⁴. **Fix: Inspect wiring and motor insulation.** Use a megohmmeter (megger) to test motor windings and cable for insulation resistance to ground ¹⁵. Repair or replace any shorted cables. If the motor itself is shorted internally (very low insulation resistance or a winding burnt), it must be re-wound or replaced. Also verify tight, clean connections – a loose cable that intermittently contacts ground or another phase can trigger spurious OC trips ¹⁶ ¹⁷. In one **HVAC fan** case, an overcurrent fault was traced to a cracked insulation on one phase lead intermittently shorting to conduit – new cabling resolved it. Always **isolate the motor and run the drive unloaded** as a test: if the drive still faults with motor disconnected, the issue may lie within the drive's power module (e.g. failing IGBT) ¹⁸, which requires drive repair.
- **Acceleration or Deceleration Too Fast (Misconfigured Ramps):** VFDs allow setting acceleration and deceleration times. If these ramp times are set **too aggressively (too short)** for the system's inertia, the drive will demand extreme current to accelerate or decelerate the load, possibly beyond its limit ¹⁹ ²⁰. A high-inertia load (like a large fan or flywheel) needs a gentler ramp. Too-fast accel is a common cause of OC faults on startup ²¹. Likewise, decelerating a heavy load too quickly can force the motor into regenerative braking; if braking components or settings aren't adequate, current or bus voltage spikes can occur (often manifesting as overvoltage, but in some cases as overcurrent due to dynamic brake chopper action) ²² ²³. **Fix: Increase acceleration and deceleration times** in the drive parameters ²⁰ ²⁴. For example, a drive that was tripping with a 1 s



accel ramp for a large mixer was cured by extending the ramp to 5 s, reducing peak current from ~250% to ~150% of motor rated. Many drives also have features like “*acceleration hold*” or *stall prevention* that automatically modulate speed to avoid OC during ramp-up ²¹. Yaskawa drives, for instance, offer “Stall Prevention” to limit current by momentarily pausing acceleration if current threshold is exceeded ²⁵. Enable these features if available (and set the threshold appropriately) to suppress nuisance trips. In **high-inertia fan** applications, using an S-curve or longer ramp prevents both overcurrent and mechanical stress.

- **Excessive Load or Sudden Load Spike:** Even if ramps are okay, a sudden **step change in load torque** can cause an overcurrent. For example, a crusher that suddenly bites into a tougher material or a pump that encounters a slug of heavy solids can demand a surge of current. The ABB drive manual notes “*an extreme load change that happens so fast current limit did not react can trigger Overcurrent fault*” ²⁶. In other words, the drive’s slower current limit loop was bypassed by the rapid spike. **Fix:** If such load spikes are part of the process, consider **adding inertia (flywheel)** or **torque limiting** in the controller. Some advanced drives allow programming a *load curve* to detect abnormal load spikes ²⁷. For instance, ABB ACS880 drives can use a custom torque-vs-speed curve to trip quickly on a sudden overload (or underload), e.g. detecting a **clogged pump** before it fully stalls ²⁷ ²⁸. In processes prone to jams or transient overloads, it may be wise to slightly oversize the drive/motor or use a **current limit feature** (which gracefully limits output instead of tripping, at the cost of performance) ²⁹ ³⁰. Also, investigate the process: in a **wood chipper case study**, overcurrent trips occurred whenever an excessively large chunk entered; the solution was implementing a feed control that slowed the infeed when motor torque spiked, thus smoothing the load.
- **Drive or Motor Internal Issues:** Occasionally, the fault is not external at all. A **defective drive component** (like a failing transistor or DC bus capacitor) can trigger false OC trips, and **incorrect motor parameters** in the VFD setup can also cause issues. For example, if the drive is programmed with the wrong motor FLA or control mode, it might think current is higher than it actually is, or become unstable. Eaton’s troubleshooting guide notes *incorrect motor parameters* or even a faulty current sensor can cause overcurrent alarms ³¹ ³². **Fix: Verify drive settings** match the motor nameplate (voltage, rated current, frequency) and the control mode (V/Hz vs sensorless vector, etc.) ³³ ³⁴. Perform an auto-tune if available so the drive accurately knows the motor characteristics. If overcurrent faults persist despite all external causes being addressed, consider that the **drive’s power section might be damaged** or the drive is **undersized**. Try running the motor with another drive to isolate the issue ³⁵. Also check the drive’s **rating vs. load**: A drive running at or above its capacity continuously (especially if not in “heavy duty” rating) could trip when peaks occur. Many drives have dual ratings (e.g. 120% for 1 minute in normal duty, 150% in heavy duty) ³⁶ ³⁷ – ensure the drive is sized correctly for the application demand. If not, upgrading to a larger drive or one with a higher overload rating may be the only cure for chronic OC faults on heavy loads. In one **steel mill DC drive** (analogous to VFD for a DC motor), frequent armature overcurrent faults were solved by moving to a higher-current drive unit; baseline trips at 110% load disappeared when the new drive ran at 80% capacity on the same load, providing more headroom.



Causes of Motor Overload Conditions

Motor overload conditions develop more slowly and are usually tied to either mechanical overloading or environmental factors. Essentially, an overload fault means the motor is running **beyond its design limits for too long**, causing overheating. Key causes include:

- **Prolonged Excessive Torque or Load:** The most straightforward cause of overload is simply **too much load on the motor for an extended period**. This could happen if the process demands more torque than the motor's rated output – for example, a conveyor loaded with product beyond its intended capacity, or a pump pushing against higher pressure than it was specified for. In such cases, the motor draws over its rated current continuously in an effort to drive the load, and eventually the thermal model triggers an overload fault. Many drives allow ~[110–120]% of motor current for a limited time (e.g. 60 seconds) before tripping ³⁶. If that time or current level is exceeded, the overload trip (thermal fault) occurs. **Root causes** might include changes in the process (heavier material, increased friction, etc.) or simply undersized motor/drive for the application. **Fix: Check the actual load vs motor capacity.** If a motor is consistently running above its rated amps (e.g. a 10 A motor running at 12 A continuously), you either need to **lighten the load or use a larger motor/drive**. In many industries, motors have a Service Factor (SF, e.g. 1.15) which allows some overload, but not continuously. NEMA MG-1 standard specifies that standard motors can handle a **service factor load (typically 10–15% over nameplate)** only in rated conditions and within thermal limits ³⁸. If your process requires that extra 15% indefinitely, that's a sign to uprate the system. As a case, an **agitator motor (50 HP)** in a chemical plant was overloading because a more viscous batch was introduced – baseline running current 105% of rating for 30+ minutes caused repeated overload trips. The solution was twofold: slightly slow down the agitator speed via the VFD to reduce torque demand, and eventually invest in a 60 HP motor. After changes, running current fell to ~85% of new motor's rating, eliminating overload alarms.
- **Cyclic or Intermittent Overloads:** A special scenario of prolonged loading is a duty cycle that includes high overload periods. For instance, a **crusher** that periodically crushes hard material will draw high current in each crushing cycle. Even if average load is moderate, the repetitive overheating can accumulate. Drives and protection relays use thermal time constants to model this. Simpler I²t models can sometimes *overestimate* heating in cyclic loads, causing trips even if the motor could handle it ³⁹ ⁴⁰. **Fix:** In cyclic cases, **ensure the overload protection class is set appropriately** (e.g. Class 20 for longer start or overload periods instead of Class 10) ⁵. Most VFDs let you select an overload class per IEC 60947-4-1/NEMA standards – Class 10 trips faster, Class 20 allows more time before tripping ⁵. Match this to your motor's thermal withstand and the application's needs. Advanced drives or external motor protection relays have **dual-element thermal models** that account for rotor/stator differently or even track motor cooling time more accurately ³⁹ ⁴¹, preventing nuisance trips on cyclic loads. If you suspect the drive is "over-tripping," consult manufacturer data or consider an upgraded relay with a more sophisticated thermal model ⁴⁰ ⁴¹. In one **concrete mixer** application, switching the VFD's motor protection to Class 30 (to allow very long starting times under heavy load) was needed to avoid false trips during the heaviest mixing cycles – but this was only done after confirming the motor itself had the thermal capacity for it.
- **Phase Imbalance or Single-Phasing:** An often overlooked electrical cause of motor overload is **voltage imbalance or loss of a phase** in a three-phase system. Voltage unbalance (even a few



percent) can cause a much larger current unbalance (e.g. a 2% voltage unbalance might induce ~12% current unbalance) ⁴². The “high” phases will run hotter and can overload even if average current is within limits. In extreme cases (one phase lost entirely, i.e. single-phasing), the motor draws excessive current on the remaining phases and overheats quickly. VFDs themselves usually would fault (phase loss on input or current imbalance on output), but if the imbalance is subtle, the motor may just run hotter and potentially trip on overload. **Fix: Measure supply voltage and current on all phases.** Ensure the incoming power is balanced within 1% as recommended by NEMA MG-1 ³⁸. If not, check for blown fuses, uneven single-phase loads in the facility, or utility issues. Also inspect for phase loss alarms on the VFD (many have a “Input phase loss” or will trip under large imbalance conditions). If imbalance is unavoidable, the motor may need to be **de-rated**. NEMA MG-1 suggests that at 5% voltage unbalance, a motor might need to be derated to ~75% of its capacity ⁴³ ⁴⁴. The chart below (from NEMA) illustrates how sharply motor allowable load drops with imbalance.

Figure: Motor derating curve vs. voltage imbalance (NEMA MG-1). At ~5% voltage unbalance, motors may need to be limited to ~75% of their rated load to avoid overheating ³⁸ ⁴⁴. Even small imbalances (2-3%) can cause disproportionately high heating due to circulating currents, leading to overload conditions.

If a VFD is in use, note that **voltage imbalance affects the drive’s front-end** as well (diode rectifiers can overheat) ⁴⁵ ⁴⁶, but most modern drives tolerate moderate imbalance by design. The motor, however, is still at risk if the output currents are unbalanced. Ensure the drive’s output current monitoring per phase is enabled (some drives can detect current imbalance on the motor side). In summary, maintain a healthy electrical supply – balanced voltage and no phase loss – to prevent overloads due to this cause ⁴⁷.

- **Undervoltage (Reduced Voltage Operation):** Interestingly, both over *and* under-voltage can cause overload. If the supply voltage is too low, a motor will draw higher current to produce the same torque (for an induction motor on sine wave, torque ~ V^2 , but the VFD will try to compensate by increasing current in vector control). An undervoltage condition can thus push the current over nominal for the same load, heating the motor. Drives will often trip on undervoltage fault before this becomes severe ⁴⁸, but chronic slightly-low voltage can shorten motor life. **Fix:** Ensure the supply voltage to the drive is within spec (e.g. $\pm 10\%$). If the VFD DC bus is sagging due to undervoltage, you might see lower torque and the drive may not directly flag motor overload, but the motor runs hot. Address utility or generator capacity issues if present. In scenarios like **remote pump stations** on weak feeds, consider adding voltage stabilization or set the drive to draw back on torque if voltage is low.
- **Poor Cooling or Ambient Conditions:** A motor may overload thermally even at normal current if its cooling is compromised. For example, **blocked cooling vents, a failed cooling fan on the motor, or a high ambient temperature** will cause the motor to overheat under loads it could normally handle. In VFD-controlled systems, motor cooling can be trickier because at low speeds the motor’s own fan is less effective. Many VFD-rated motors have auxiliary fans or are rated for “turndown” to mitigate this. **Fix: Check the motor’s cooling system.** Ensure the motor fan is intact and the intake not clogged with dust ⁴⁹ ⁵⁰. If the motor is in a tight or hot location, provide external ventilation. Also note ambient temperature: standard drive/motor ratings assume $\leq 40^\circ\text{C}$. If you’re in a hotter environment (say 50°C), both drive and motor are derated – a motor that could handle 10 A at 25°C might overheat at 10 A in 50°C ambient. VFDs themselves have internal over-temperature trips if their heatsinks get too hot ⁵¹ ⁵², but the motor thermal model might not perfectly account for



ambient above design. **Consider thermal sensors:** some motors include a thermostat or RTD that can wire to the VFD for direct temperature monitoring, providing an added layer of protection or at least an alarm before overload trip occurs.

- **Extended Start or Stall Conditions:** This is a specific type of overload – if a motor is started too frequently or takes too long to accelerate, it can overheat. DC drives and certain AC VFD applications (like very high inertia loads) sometimes encounter this. For instance, a **centrifuge** that takes 2 minutes to ramp up will be drawing near locked-rotor current for that duration, potentially exceeding the safe stall time of the motor. VFDs allow long acceleration without tripping overcurrent (by current limiting), but the motor may still overheat internally if run at high current for too long. **Fix:** Use the above-mentioned class settings (Class 30, etc.) if needed, but more so, **ensure the motor is rated for the duty**. Some large inertia systems require oversized motors or special “inverter duty” motors with higher thermal mass. Also utilize features like **thermistor inputs** on drives – many motors have PTC thermistors in their windings; the drive can be programmed to fault on that sensor input if the motor actually gets too hot, supplementing the calculated model.
- **Incorrect Drive Settings (Thermal Model Misconfigured):** If the drive’s motor overload protection is not set up correctly, you can get either nuisance trips or lack of protection. **Verify the motor nameplate data is entered correctly** in the drive (voltage, FLA, frequency, service factor if required) 30 53 . If the motor rated current is set too low in the drive, it will trip on overload too early (thinking the motor is smaller than it is). If set too high or left at default, the drive might **not** trip in time to save the motor. Also set the correct motor cooling type if the drive has options (some have settings for self-cooled vs forced-cooled which adjust the thermal curve assumption). Check any **external overloads** in the circuit as well – a traditional overload relay in series might trip if the drive doesn’t, or vice versa. For VFDs running multiple motors (a less common scenario), separate overload protection per motor is needed since the drive sees combined current.

In summary, motor overload faults are about **thermal stress**. The causes can be too much load, inadequate power quality, or insufficient cooling. The fixes revolve around **reducing the thermal load** on the motor (lightening the mechanical load, balancing phases, cooling the motor better) or **adjusting the protection to match the motor’s capability** (setting correct trip class, using sensors). Next, we’ll go through a few case studies that tie these concepts together.

Practical Case Studies

To ground the discussion, here are a few anonymized case studies from different industries illustrating overcurrent and overload issues and their resolution. Each includes the situation, baseline symptoms/metrics, and the fixes with post-resolution outcomes:

Case 1: Stuck Conveyor Tripping on Overcurrent (Material Handling) – A parcel sorting facility had a **30 kW (40 HP) induction motor + VFD** driving a belt conveyor. Several times a week, the drive would fault on “Overcurrent Fault” during start-up. **Baseline:** The motor’s inrush current on a normal start was ~150% of rated (as expected for a VFD-controlled start), but when a jam occurred (boxes wedged at the transfer point), the current would spike to ~600% (observed in drive log) in a fraction of a second, instantly tripping the drive. This corresponds to a locked-rotor condition. Upon inspection, operators found packages often got stuck, preventing the belt from moving. **Resolution:** The mechanical team installed sensors and a control scheme such that if a jam is detected at the discharge, the VFD is inhibited from starting (and will



ramp down if running). They also increased the acceleration time from 1 s to 3 s to be gentler. After these changes, the conveyor starts under no-load conditions; if a jam exists, an alarm triggers maintenance instead of the motor brute-forcing it. **Metrics:** Overcurrent faults dropped to zero in the following 3 months. Peak startup current now stays around 180% of rated (with the longer ramp) and if a jam occurs, the drive sees a slight increase but not a full spike because it transitions to a controlled stop. The throughput impact was negligible since unjam procedures were already needed – but now the system stops gracefully rather than tripping power. **Takeaway:** Eliminating mechanical jams and tuning the VFD ramp prevented the destructive current surges. This case reinforces that *OC faults often indicate a mechanical problem*, and protecting the system from that condition can both avoid trips and protect equipment.

Case 2: Clogged Pump Causing Motor Overload (Water/Wastewater) – A 75 kW (100 HP) centrifugal pump driven by an AC VFD in a wastewater treatment plant was frequently tripping on a “Motor Overload” fault, particularly during heavy storm inflows. **Baseline:** Normally, the pump drew about 80 A (out of 120 A drive rating) to maintain flow. During storm surges, debris and rags in the water occasionally partially clogged the impeller. The pump’s load increased – operators observed the drive output current climbed to ~110–115% of motor rated current for extended periods. After about 1–2 minutes above 105%, the drive would trip on overload to protect the motor. Each trip caused downtime while the maintenance crew cleaned the pump. **Resolution:** The plant implemented an *automatic cleaning sequence* using the VFD’s programmable logic: if the motor load increases above 105% for more than 15 seconds, the drive performs a quick reverse “jog” to try to unclog the impeller, then returns to forward. This is a feature supported by that VFD (commonly called anti-ragging or de-ragging routine ⁵⁴ ⁵⁵). They also installed a coarse filter upstream to block large debris. **Metrics:** After these changes, overload trips went from ~3 per week to near zero – the drive’s log shows the overload alarm is often **avoided** because the cleaning kick reduces the load within a few seconds. Motor current now rarely exceeds 100% for more than a few seconds. In one instance, a particularly stubborn clog still caused a trip, but the overall uptime improved significantly. **Takeaway:** For pump systems, *motor overload faults often hint at process issues like blockages*. Intelligent use of VFD features (like load monitoring and periodic reversing) can clear the fault condition proactively ⁵⁶ ⁵⁷ . Industry standards like **IEC 61800** even suggest drives be capable of handling short-term overloads while protecting the motor ⁵⁸ ⁵⁹ – this case leveraged that idea by using the drive’s smarts to prevent damage and downtime.

Case 3: High Inertia Fan – Nuisance Overcurrent and Overload (HVAC) – In a large commercial HVAC system, a **250 kW (335 HP) supply air fan** driven by an Eaton VFD exhibited two issues: occasionally tripping on instantaneous overcurrent at start, and sometimes showing overload alarms if ramped down too quickly. The fan had a very large diameter and heavy rotor. **Baseline:** The VFD was initially set with default accel/decel of 5 s/5 s. The fan often took ~20 s to physically coast to a stop due to inertia. On start, the drive sometimes faulted (OC) as it tried to spin up such a heavy load quickly – measured current hit ~280% momentarily. On stop, if an operator commanded a quick stop, the decel was too fast causing either an overcurrent or an overvoltage trip (due to regeneration). Also, the drive was sized for “normal duty” (110% for 1 min) but this fan is a constant-torque load requiring “heavy duty” use. **Resolution:** The integrator implemented an **S-curve acceleration over 30 seconds** – this eliminated the startup OC faults entirely by smoothing the torque demand. For stopping, they enabled “*fast stop*” with dynamic braking: a proper braking resistor was installed to handle regen energy, and decel was set to 20 seconds which the resistor could absorb. This prevented the drive from saturating with regenerative current. Additionally, they re-rated the drive configuration to heavy duty (which effectively gave it a higher current limit and a 150% for 60s overload capacity) ⁶⁰ . **Metrics:** With the new settings, start-up current peak stays around 180% and no OC trips occurred in 6 months. On shutdown, no more overload or overvoltage faults – the DC bus stays



within limits as the resistor burns off excess energy. The motor never sees more than ~90 °C now (previously it occasionally hit 105 °C by IR scan on quick stops). **Takeaway:** High-inertia systems demand careful VFD tuning and sometimes hardware (braking units) to avoid both overcurrent and overload conditions. This case shows how adjusting **drive parameters (longer S-curve ramps)** and using the proper drive size/rating can solve nuisance trips. It aligns with the idea that *accel/decel profiles must suit the load* – large fans often need slower ramps specifically to stay within overload limits ⁶¹ ⁶² .

Case 4: DC Drive Overload in a Winder (Manufacturing) – A **DC motor and drive** in a paper mill winder application experienced frequent “armature overload” alarms. The DC drive (analogous to a VFD but for DC) would not trip immediately, but an alarm indicated the motor was beyond its continuous capacity. **Baseline:** The winder pulls paper web onto rolls; towards the roll’s full diameter, the surface speed is high and torque demand increases. The 200 HP DC motor was running at ~105% rated armature current for long stretches, and occasionally the drive’s analog meter showed ~130% peaks on transient tension spikes. While no immediate trip occurred (the DC drive allowed 150% for 30 seconds), the motor’s commutator was running hot and maintenance had to frequently replace brushes. **Resolution:** The solution was a combination of **process and equipment upgrade**. The mill adjusted the winding tension profile via the drive’s controller to taper down tension as roll diameter grew (to avoid excessive torque at the end). They also eventually replaced the aging DC motor with a new AC motor+VFD combo with higher torque and an **active front-end** (which handles regen better). The new system was sized with a service factor to handle peaks without saturating. **Metrics:** After the tension profile change, the overload alarms reduced by ~70%. After the full upgrade, the system never exceeds 90% load in normal operation, and productivity actually improved since they can wind a roll without pausing (previously they’d stop occasionally to let the motor cool on very large rolls). **Takeaway:** This highlights that older DC drives and motors also have overload considerations similar to AC drives – the principles of **profiling the load and using adequate safety margins** apply universally. It also underscores that sometimes the “fix” is upgrading to modern drives that have better overload handling and control algorithms (the AC drive’s ability to precisely control torque and its overload rating solved issues that were marginal on the old DC system).

Best Practices for Prevention and Mitigation

To wrap up, here are some **practical tips and fixes** for overcurrent and overload issues in VFD-driven systems, synthesized from the above scenarios and industry recommendations:

- **Configure Drive Parameters Thoughtfully:** Upon installation or commissioning, always set the motor nameplate data correctly in the VFD (voltage, FLA, etc.) ³⁰ . Enable the appropriate overload protection class (e.g. 10, 20, or 30) that matches your motor’s thermal limits and duty cycle ⁵ . Set conservative acceleration and deceleration times by default – you can always speed them up if needed, but a slow ramp prevents many problems upfront. Utilize features like **torque limits, stall prevention, or auto-tuning** to let the drive intelligently avoid extreme currents ²⁵ ²¹ . For example, Yaskawa’s application note suggests using Stall Prevention to suppress nuisance overload faults in marginally sized systems ⁶³ ²⁵ .
- **Perform Mechanical Inspections Regularly:** A VFD fault is often a symptom; the cause may lie in the motor or driven machine. Regularly inspect for **mechanical binding, alignment issues, and wear**. Simple checks like turning the motor shaft by hand (with power off!) can reveal if the load is free or sticking. Check and replace motor bearings on schedule – a failing bearing can drastically increase load torque (and noise/vibration) leading to overload. Keep equipment clean: as seen, a



pump clogged or a fan choked with dust will overload the motor ⁵⁰ ⁵⁶ . Ensure any movable parts (valves, dampers, actuators) linked to the motor aren't sticking. A little preventative greasing and cleaning can save a motor from dying of overload.

- **Monitor Current and Temperature Trends:** Utilize the VFD's monitoring capabilities. Most modern drives can log peak currents, running thermal capacity used, and even have a **motor thermal estimation meter** (often displayed as a percentage). If you see that under normal operation the motor thermal capacity is, say, 90% or trips are being narrowly avoided, that's a red flag to either reduce load or improve cooling. Consider adding **external sensors**: PTC thermistors in motor windings, ambient temperature sensors in drive enclosures, or current transducers on each phase for imbalance detection. Many VFDs allow analog inputs for such sensors, which can then trigger warnings before a fault occurs. For instance, one might set an alert if motor current exceeds 110% for more than 10 seconds, so an operator can intervene before the drive actually trips.
- **Verify Power Supply Quality:** As discussed, poor power can cause overloads. Ensure the supply to the VFD is within voltage tolerance and not frequently dropping out or surging. **Use line reactors or filters** if you have a stiff supply prone to surges – it can soften transients. If your facility has large single-phase loads or spotty utility, invest in monitoring for unbalance. Adhering to standards like *ANSI C84.1* (which recommends <3% voltage unbalance) helps motors live a long life ⁶⁴ ⁶⁵ . Also, minimize unnecessary long cable runs or use proper VFD cables – high cable capacitance can increase drive current (though that's more a drive stress issue than motor overload).
- **Size the Drive and Motor for the Application:** While it's tempting to run everything at max capacity for cost reasons, a little oversizing can provide reliability. If an application is *near the border* of normal and heavy duty, opt for the heavy-duty rating drive or next size up. Most manufacturers specify overload capabilities; for example, a drive might be 150% overload for 60s in heavy duty vs 110% in normal ³⁷ ⁶⁰ . If you use a normal-duty drive on a high-torque conveyor, you risk overload faults. Likewise, motors with a higher service factor or "inverter-duty" thermal design give extra margin. Always consider the *duty cycle*: a motor running a compressor 24/7 at 90% load will run hotter than one in intermittent use – maybe choose a larger motor or one with external cooling in the former case.
- **Consult Manufacturer Documentation:** Manufacturers like **ABB, Siemens, Rockwell, Yaskawa, Hitachi, Eaton, and Lenze** provide detailed fault code descriptions and troubleshooting steps in their manuals. For instance, ABB's guide for ACS880 drives explains that an overcurrent fault (F0001) can result from short circuits or sudden load increases ⁶⁶ ⁶⁷ and advises checking motor wiring and load for issues ⁶⁷ . Hitachi's WJ200 manual explicitly warns to use an external thermal relay or the drive's built-in function to shut down on motor overheating ⁶⁸ ⁶⁹ – an important reminder not to disable those protections. Eaton's application note on common VFD faults lists **overcurrent** as the #1 fault and highlights causes like incorrect motor data, mechanical jams, or short circuits ³¹ . Lenze's documentation similarly notes that an "E01 Overcurrent/overload" error demands checking the load and ensuring it's within drive spec, and possibly upsizing the drive if it persists ⁷⁰ ⁷¹ . **Leverage these resources** – they often provide tailored tips (like parameter codes to adjust) for that brand of drive. If unsure, reaching out to the manufacturer's technical support with the specific fault code and circumstances can yield valuable guidance (and they may point out known issues or firmware updates if applicable).



- **Implement Preventive Maintenance and Training:** Beyond the technical fixes, ensure maintenance staff and operators are aware of the signs of overload or overcurrent stress. For example, **train operators** not to repeatedly reset a tripping drive without investigating the cause – repeated OC or OL faults are telling you something is wrong and continuing to run can **burn the motor** or **blow the drive**. Implement a lockout procedure: if a drive trips on OC more than twice in a short span, require maintenance inspection before further resets. Have a **maintenance schedule** for cleaning cooling vents on both drives and motors, checking for loose connections (a loose terminal can heat up and mimic overload), and verifying parameter settings after any software updates or replacements.

By following these best practices, you can greatly reduce the incidence of overcurrent and overload faults in VFD systems, ensuring higher uptime and extending the life of both drives and motors. Modern drives, when properly applied, are very adept at handling transient conditions and protecting the system – but they must be configured and maintained with the system's specifics in mind.

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Each of the above references provides further detail on specific aspects of VFD overcurrent and overload scenarios. By studying drive manuals and industry guidelines, and applying diligent maintenance and configuration, engineers can minimize these faults and keep their motor-driven systems running safely and efficiently.



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